Design-space reduction with super parameters for faster optimization

Hedi Böttcher, Carsten Fütterer, Stefan Harries

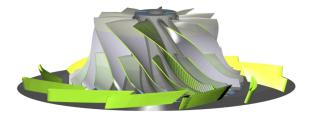
CAESES Users Meeting 2019 – Berlin, September 20th, 2019

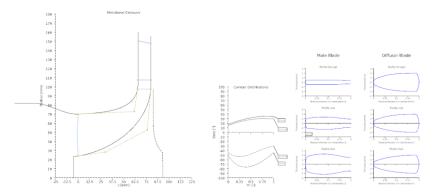
Advanced Turbomachinery Design (GAMMA)



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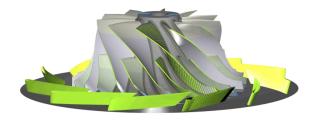




Motivation for massive parameter reduction

Problem:

- Optimization of parametric models with many free design variables requires many simulations
- Number of designs required ~ (number of free variables)²
- Aim:
 - Reduction of the number of free variables
 - \rightarrow Reduce the design space further
 - → Substantial speed-up in simulation-driven design (SDD)
- Application:
 - Design task with many free variables
 - Design tasks with long (resource-intensive) simulations



Major issue

37.5 50 62.5 75 87.5 100 112 129

In order to understand design spaces a high number of variants needs to be studied \rightarrow estimate being the square of a system's degree-of-freedom

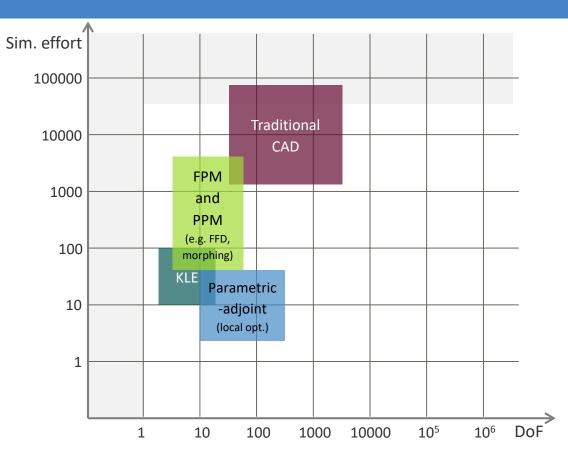
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170 160

150 140 130

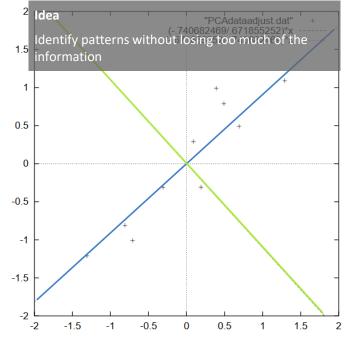
Motivation



Design-space reduction by Karhunen-Loève Expansion (KLE)

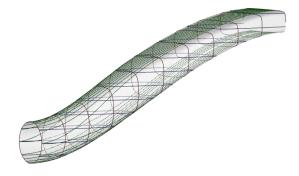
Karhunen-Loève Expansion (KLE)

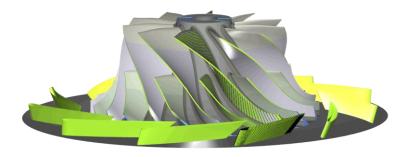
- Principle components analysis
 - A large number of statistical variables are being replaced by an approximation with a reduced number of linear combinations of orthogonal basis functions
 - Modes relate to "super parameters"
 - Decorrelation of data (as far as possible)
- Benefits
 - Check quality of a parametric model
 - If needed and possible reduce number of free variables (further)
- Aim
 - Finding an optimal basis of orthonormal functions
 - Optimality condition refers to the geometric variance retained by the new basis functions



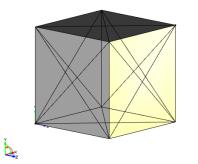
Source: Lindsay I. Smith (2002) A Tutorial on Principal Components Analysis

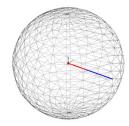












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Variability reached by super parameters

		Modified sphere	Cuboid	HVAC duct
Number of free variables of the original CAD model (DoF)		2*	3	14
Number of Sobol variants used for KLE	100	100	1000**	
Variability reached with 1 st super parameter	1	100.0 %	35.83 %	83.84 %
Variability reached with 1 st and 2 st super parameters	2	_	69.28 %	Cuboid
Variability reached with the first three super parameters Variability reached with the first four super parameters Variability reached with the first five super parameters		_	100.0 %	All CAD variables are completely independent \Rightarrow
		_	-	KLE does not give any benefit
		_	-	98.51 %
Variability reached with the first 10 super parameters	10	_	-	99.72 %
Number of super parameters needed to reach more than 95 % variability				3
Number of super parameters needed to reach more than 99 % variability				
Ratio of number of free variables of the original CAD model and number of KLE variables needed to reach 95 % variability <i>[square]</i>				67 1.8]
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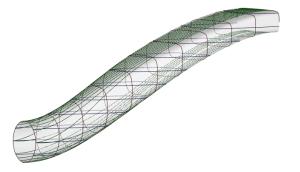
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Variability reached by super parameters

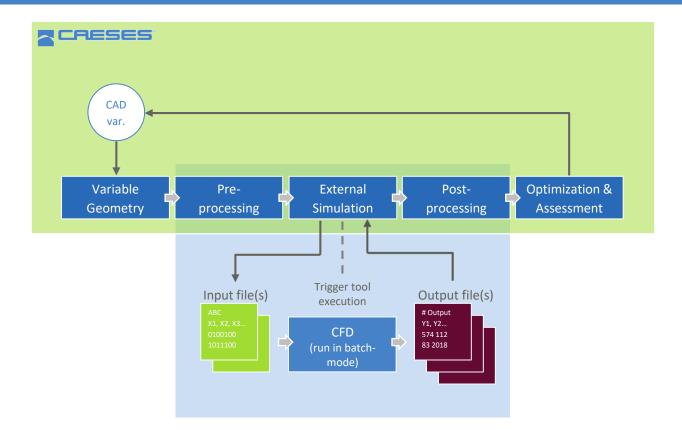
		Modified sphere	Cuboid		
Number of free variables of the original CAD model (DoF)		2*	3		
Number of Sobol variants used for KLE		100	100		
Variability reached with 1 st super parameter	1	100.0 %	35. Modi	fied sphere	with $x_1 + x_2 = r$
Variability reached with 1 st and 2 st super parameters	2	-	^{69.1} CAD v	variables are	e completely redundant \Rightarrow
Variability reached with the first three super parameters	3	-	100 KLE di	agnoses de	ependencies
Variability reached with the first four super parameters	4	-	—		
Variability reached with the first five super parameters	5	-	—		
Variability reached with the first 10 super parameters	10	-	—		
Number of super parameters needed to reach more than 95 % variability		1	3		
Number of super parameters needed to reach more than 99 % variability		1	3		
Ratio of number of free variables of the original CAD model and number of KLE variables needed to reach 95 % variability [square]		2 [4]	1 [1]		

Variability reached by super parameters

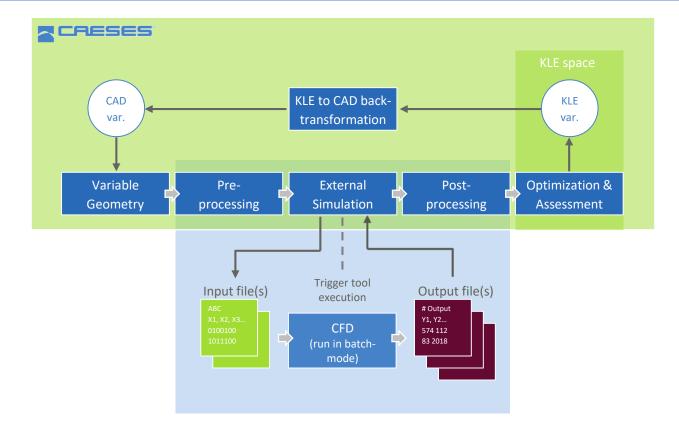
		Modified sphere	HVAC duct	
Number of free variables of the original CAD model (DoF)	•	2*	14	-
Number of Sobol variants used for KLE		100	1000**	-
Variability reached with 1 st super parameter	1	100.0 %	83.84 %	-
Variability reached with 1 st and 2 st super parameters	2	_	92.05 %	-
Variability reached with the first three super parameters	3	_	95.76 %	
Variability reached with the first four super parameters	4	—	97.44 %	-
Variability reached with the first five super parameters	5	_	98.51 %	-
Variability reached with the first 10 super parameters	10	—	99.72 %	Z
Number of super parameters needed to reach more than 95 % variability		1	3	v llex
Number of super parameters needed to reach more than 99 % variability		1	7	
Ratio of number of free variables of the original CAD model and number of KLE variables needed to reach 95 % variability <i>[square]</i>		2 [4]	4.67 [21.8]	Ţ.



Standard process



Process with KLE



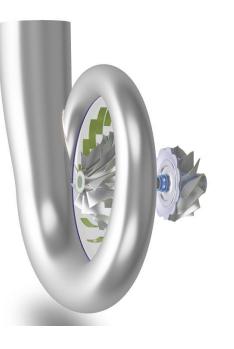
KLE for compressor optimization

Parametric Model of a Turbocharger

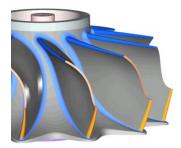


Volute Compressor

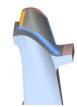




Radial turbine



Axial turbine



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Compressor Component – Impeller and Diffuser

- Geometry created in CAESES:
 - D_Out: 195mm
 - No splitter blades
 - 11 impeller blades
 - 19 diffuser blades
 - 16 design variables for the main blade
 - 10 design variables for the diffuser vane

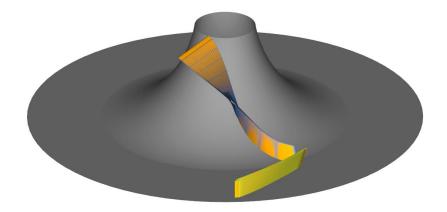
- Target:
 - Increase efficiency
- Constraint:
 - Pressure ratio > 2.1
 - Convergence

IE	
e	

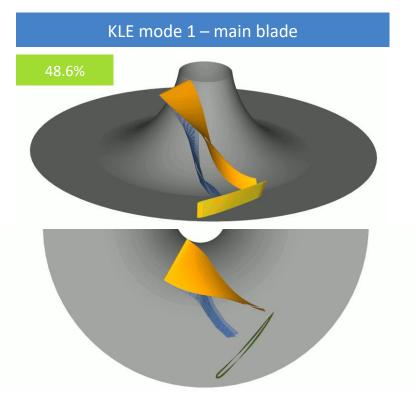
	Design Variable		Lower	Value	Upper
1	ANGLE_HUB	•	-10	0	10
2	ANGLE_SHROUD	•	-10	0	10
3	MID_SHIFT_DELTA	•	-2	0	2
4	MID_SHIFT_POS	•	0.3	0.5	0.8
5	BETA_HUB_LE	•	40	45	50
6	BETA_HUB_TE	•	45	50	55
7	BETA_SHROUD_LE	•	25	30	35
8	BETA_SHROUD_TE	•	40	41.7	50
9	BETA_TanFactor_HUB_LE	•	0.4	0.5	0.6
10	BETA_TanFactor_HUB_TE	•	0.4	0.5	0.6
11	BETA_Tan_HUB_LE	•	-45	-45	-35
12	BETA_Tan_HUB_TE	•	-65	-60	-55
13	BETA_TAN_SHROUD_LE	•	-15	-10	-5
14	BETA_TAN_SHROUD_TE	•	-40	-35	-30
15	THETA_DELTA_SHROUD_LE	•	-10	-2	0
16	THETA_DELTA_SHROUD_TE	•	-10	0	10
17	Diff_BETA_HUB_LE	•	17	19	25
18	Diff_BETA_HUB_TE	•	28	37	44
19	Diff_BETA_SHROUD_LE_Delta	•	-4.5	-2	3.5
20	Diff_BETA_SHROUD_TE_Delta	•	-5	-1	8
21	Diff_BETA_Tan_HUB_LE	•	-30	-20	-10
22	Diff_BETA_Tan_HUB_TE	•	-7.5	0	10
23	Diff_BETA_Tan_SHROUD_LE	•	-30	-20	-10
24	Diff_BETA_Tan_SHROUD_TE	•	-10	10	20
25	DIFF_THETA_DELTA_SHROUD_LE	•	-15	-3	8.5
26	DIFF_THETA_DELTA_SHROUD_TE	÷	-5	0	5

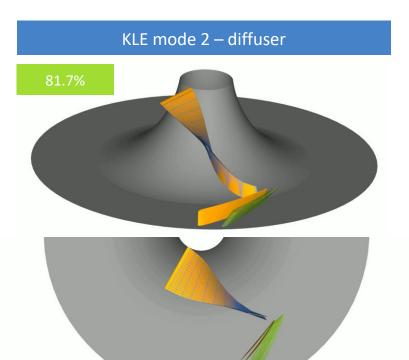
Building a KLE model

- 1) Build a parametric model (as usual)
- 2) Produce an ensemble of variants (DoE)
 - Same topology, different geometry
- 3) Determine KLE \rightarrow Generate the KLE model
- 4) Decide how many KLE variables shall be used
- 5) Optimize in KLE space
 - Generate new variant in KLE space
 - Back-transform from KLE space to CAD space and analyze (and repeat)

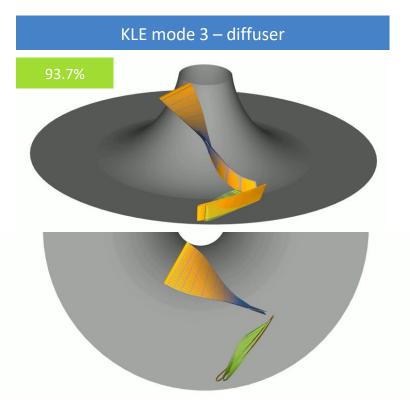


First and second KLE modes

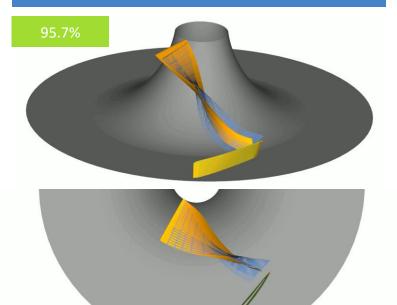




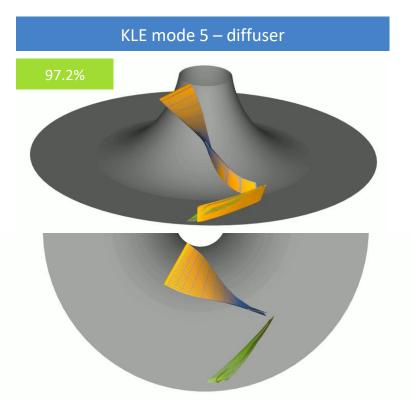
Third and fourth KLE modes



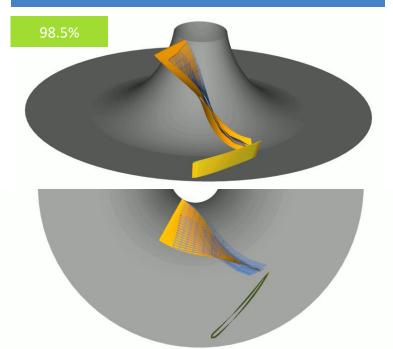
KLE mode 4 – main blade



Fifth and sixth KLE modes



KLE mode 6 – main blade



Compressor Component – CFD setup

NUMECA NUMECA Software: AutoGrid5[™] for hexahedral grid – FINE[™]/Turbo for CFD computation NUMECA

20

Setup:

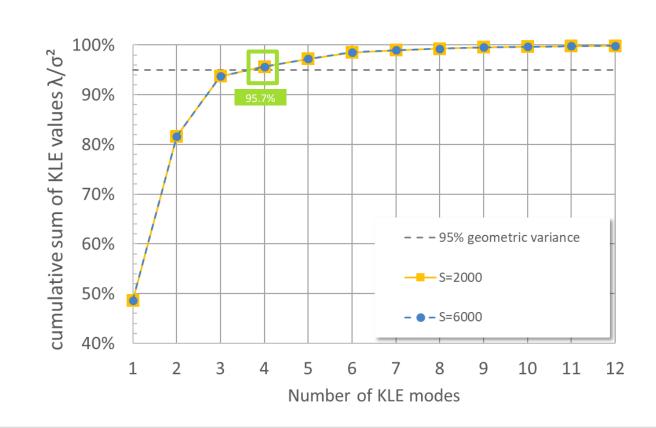
generation

- Revolutions per min: 37,000
- Mass flow rate: 1.35kg/s

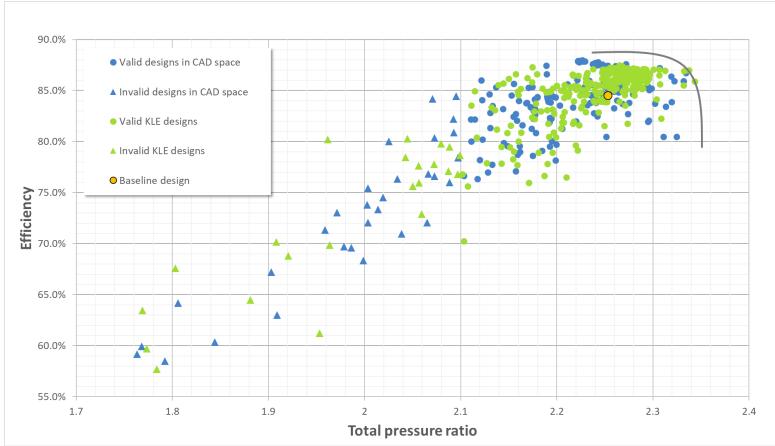


Optimization in KLE space

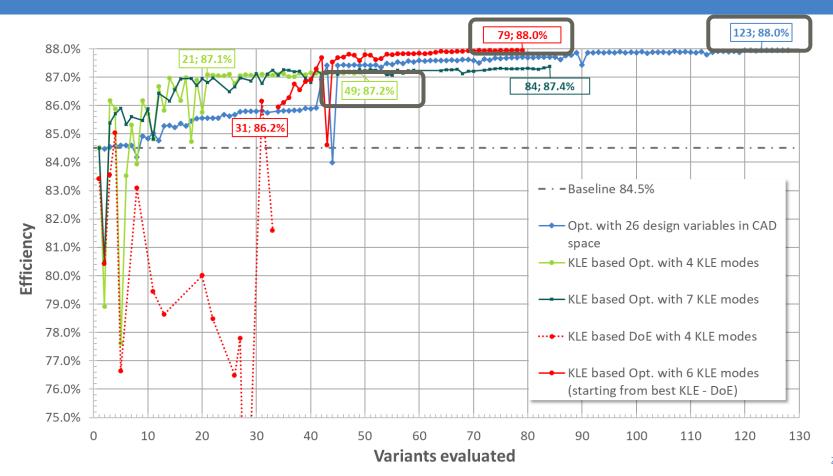
Variability with each KLE mode



Results for total pressure ratio and efficiency

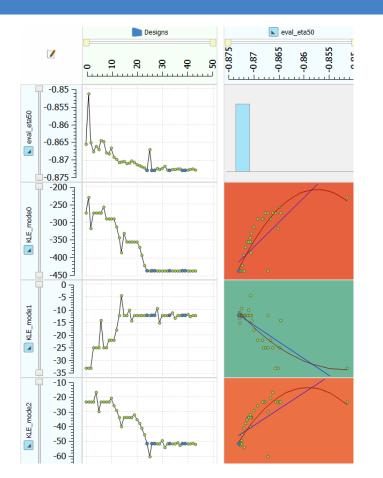


Optimization history for the compressor



2019

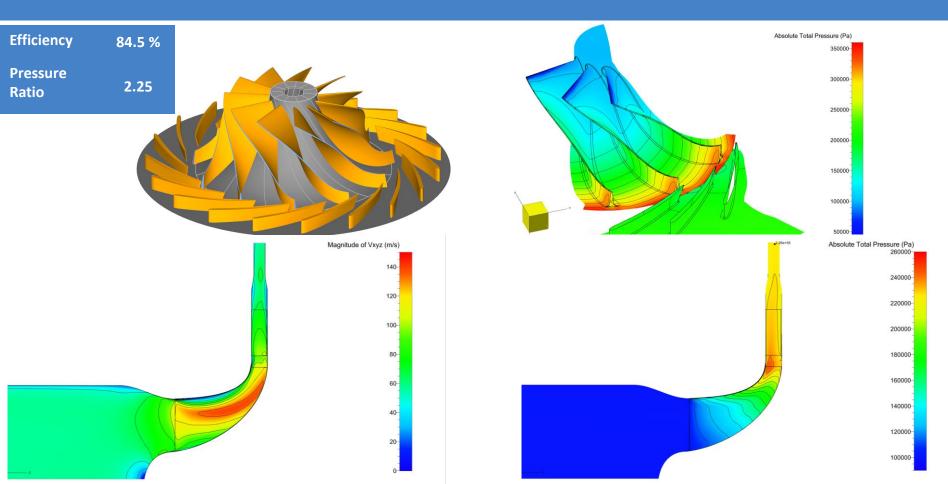
Optimization in KLE space



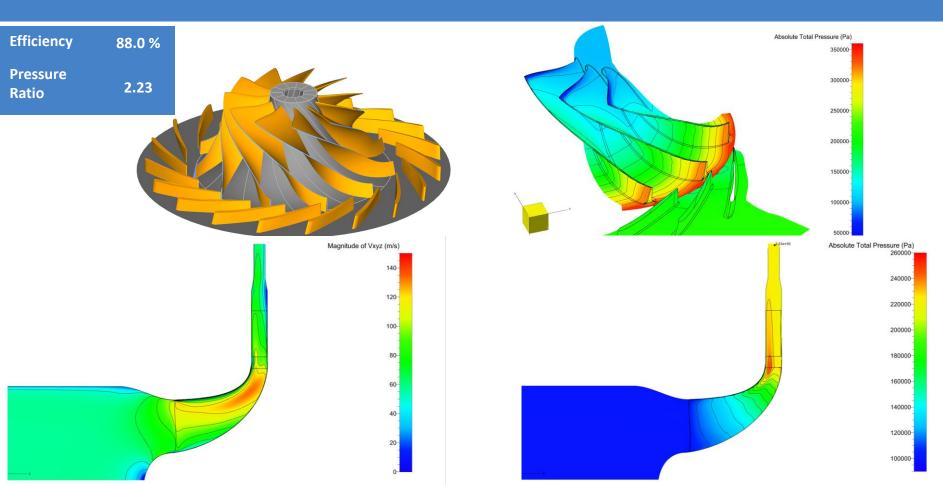
- Optimization in CAD space with 26 design variables for comparison
 - Starting from the baseline design
 - 128 variants evaluated with 3.5% improvement

- Optimization in **KLE space** with **4 KLE modes**
 - Starting from the baseline design
 - 49 variants evaluated with 2.7% improvement
- Optimization in **KLE space** with **6 KLE modes**
 - Starting from the best DoE result (4 KLE modes)
 - 79 variants evaluated (33 DoE + 46 Opt. designs)
 - 1.7% + 1.8% = **3.5%** improvement

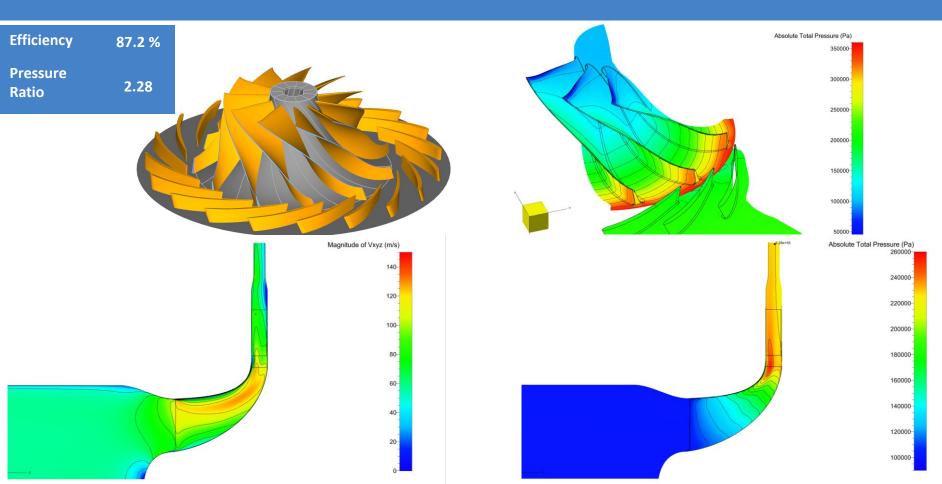
Baseline



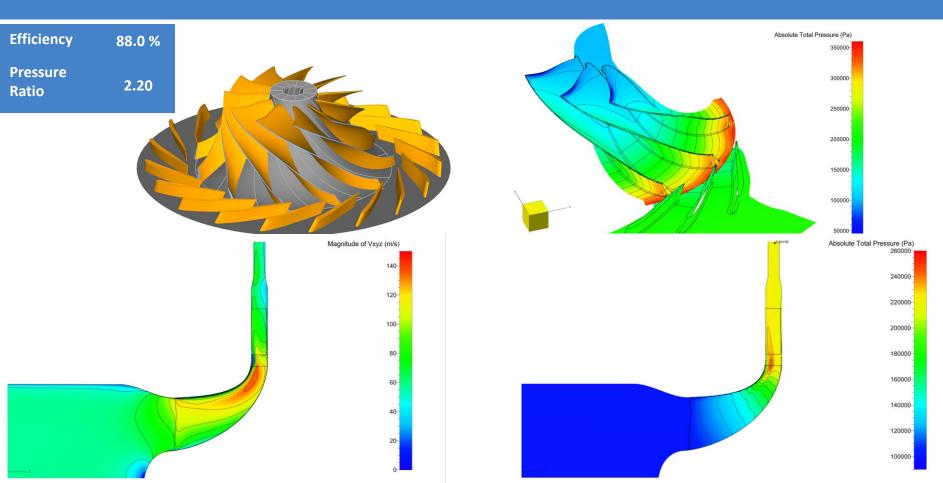
Des 123 – Best Opt. With 26 Design Variables



Des 049 – Best KLE based Opt. with 4 KLE modes

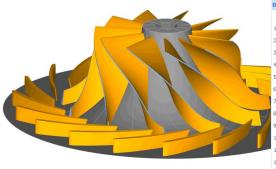


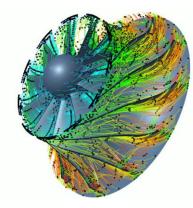
Des 079 – Best KLE based Opt. with 6 KLE modes (best DoE start)



Conclusions

Conclusion





						KLE mode 1 – main blade	KLE mode 2 – diffuser
Des	sign Variables					KLE HIOUE I – HIAIII DIAUE	KLE MOUE Z – umuser
	Design Variable		Lower	Value	Upper	40 60/	
1	ANGLE_HUB	*	-10	0	10	48.6%	81.7%
2	ANGLE_SHROUD	•	-10	0	10		
3	MID_SHIFT_DELTA	*	-2	0	2		
4	MID_SHIFT_POS	*	0.3	0.5	0.8		
5	BETA_HUB_LE	•	40	45	50		
6	BETA_HUB_TE	*	45	50	55		
7	BETA_SHROUD_LE	*	25	30	35		
8	BETA_SHROUD_TE	•	40	41.7	50		
9	BETA_TanFactor_HUB_LE	*	0.4	0	0.6		
10	BETA_TanFactor_HUB_TE	*	0.4	0	8		
11	BETA_Tan_HUB_LE	*	-45	-	-05		
12	BETA_Tan_HUB_TE	*	-65	- 0	-55		
13	BETA_TAN_SHROUD_LE	*	-15	-			
14	BETA_TAN_SHROUD_TE	*	-40	-35	-30	KLE mode 3 – diffuser	KLE mode 4 – main blade
15	THETA_DELTA_SHROUD_LE	*	-10	-2	0		
16	THETA_DELTA_SHROUD_TE	•	-10	0	10	93.7%	95.7%
17	Diff_BETA_HUB_LE	*	17	19	25		55.770
18	DIFF_BETA_HUB_TE	*	28	37	44		
19	Diff_BETA_SHROUD_LE_Delta	•	-4.5	-2	3.5	Massive parame	ter reduction
20	Diff_BETA_SHROUD_TE_Delta	*	-5	-1	8		
21	Diff_BETA_Tan_HUB_LE	*	-30	-20	-10	26 design variah	es can be reduced to 4 KLE modes
22	Diff_BETA_Tan_HUB_TE	•	-7.5	0	10	20 design variab	es can be reduced to 4 KLL modes
23	Diff_BETA_Tan_SHROUD_LE	*	-30	-20	-10	retaining more t	nan 95% of the original variance
24	Diff_BETA_Tan_SHROUD_TE	*	-10	10	20	retaining more t	an observe on the onginar variance
25	DIFF_THETA_DELTA_SHROUD_LE	•	-15	-3	8.5	Bird 2	
26	DIFF_THETA_DELTA_SHROUD_TE	*	-5	0	5		

Conclusions

- The less free variables to work with the better
- An approach has been developed with which to substantially reduce design spaces made of CAD variables by mapping them into spaces spanned by a different kind of variables, dubbed super parameters
- A back-transformation from KLE to CAD space is needed for complex models
- Massive parameter reduction for faster fluid-dynamic optimization of shapes were shown

- Outlook and future work:
 - Combine parametric-adjoint solutions with KLE (sensitivity analysis)

Promising combination

High-level parametric models with further parameter reduction

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 (www.caeses.com).

References



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